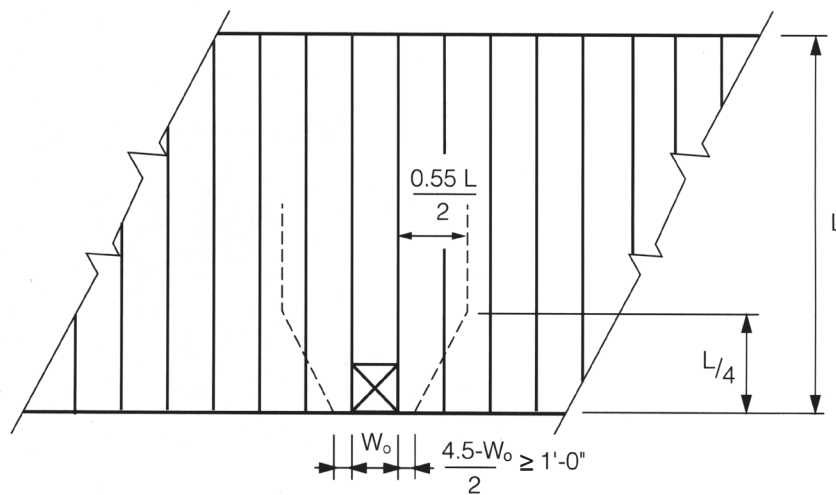


SHEAR DESIGN AT END OPENINGS

Research on load distribution has been a major part of the continuing testing program conducted by the Spancrete Manufacturers Association.



EFFECTIVE RESISTING SLAB WIDTH AT END OPENINGS

CONCLUSIONS:

1. Openings at the end of a span will cause a concentration of shear stresses due to shear and torsion at the sides of an opening.
2. The midspan region will not be affected by an end opening as long as strand development occurs after the opening and before the area of maximum moment.
3. The effective resisting section shown is recommended for shear design around end openings. The design procedure is to superimpose on the uniform loads the distributed load concentrations.

A design example is given on the reverse side.

SHEAR DESIGN AT END OPENINGS

GIVEN:

An 8" x 40" Spancrete® hollowcore system as shown.
 Self-weight = 64 psf, uniform superimposed
 dead and live loads are 10 psf and 40 psf

PROBLEM:

Select the prestress, check strand
 development, and check shear.

SOLUTION:

- From load tables, for a total superimposed load of 50 psf, select eight 5/16" dia. 250 ksi strands with 3/4" clear cover. Use 65% for initial tension and assume 20% losses, and concrete strength of 5000 psi
- Check strand development from opening

$$L_d \text{ required} = (f_{ps} - 2/3f_{se}) d_b = (.98 \times 250 - 2/3 \times .65 \times .8 \times 250)/16 = 50"$$

$$L \text{ available} = \left(\frac{25}{2} - 3\right)12 = 114" > 50" \text{ OK}$$

- Check shear caused by the additional concentration of load from the strip of slab containing the opening.

Plank bearing = 4"

$$\text{At } h/2, \text{ distribution width } DW = 1 + \frac{.333}{6.25} \left(\frac{13.75}{2} - 1\right) = 1.31'$$

$$W_u = 1.2(10 + 64) + 1.6(40) = 153 \text{ psf from uniform loads}$$

Distribute load from strip with opening and superimpose

$$W_u = 153 + \left(\frac{153 \times 3.33}{1.31 \times 2}\right) = 348 \text{ psf}$$

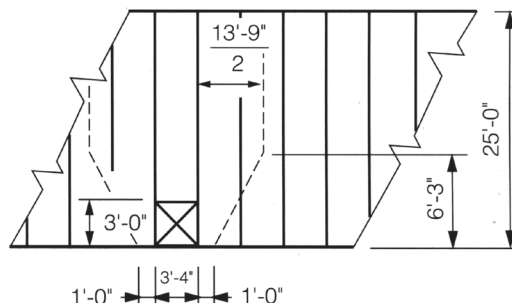
Checking shear at critical points, find:

$$\phi v_{cw} = 203 \text{ psi} > v_u = 118 \text{ psi and } \phi v_{ci} = 106 \text{ psi} > v_u = 78 \text{ psi. Shear check is OK.}$$

- If inclined shear had not checked at some point in the span, calculate a new effective width at that point, determine a new distributed load, and recheck shear.

Additional information for Shear Design is provided in Research Note title, "SHEAR STRENGTH"

Note: Sample calculations are intended to illustrate the concept presented and do not represent all considerations necessary for the complete design. This research was done using 40" wire, 8" thick Standard Spancrete. However, this concept applies to all Spancrete cross sections.



MIDWEST

Hanson Structural
 Precast Midwest, Inc.
 Maple Grove, Minnesota

Spancrete, Inc.
 Green Bay, Wisconsin

Spancrete Industries, Inc.
 Waukesha, Wisconsin

Spancrete of Illinois, Inc.
 Arlington Heights, Illinois

Wells Concrete
 Wells, Minnesota

WEST

Hanson Structural
 Precast Pacific, Inc.
 Irwindale, California

KIE-CON

Division of Kiewit Pacific Co.
 Anitoch, California

Owell Precast
 Sandy, Utah

SOUTHWEST

Manco Structures, Ltd.
 Schertz, Texas

SOUTH

Cement Industries, Inc.
 Fort Myers, Florida

Florida Precast Industries, Inc.
 Sebring, Florida

EAST

Mid-Atlantic Precast, LLC.
 King George, Virginia

EGYPT

Samcrete Egypt
 Ahram, Giza

MEXICO

ITISA
 Mexico City, Mexico

Spancrete Noreste
 Monterrey, Mexico

CROATIA

Mucic & Co
 Dugopolje, Croatia

CARIBBEAN

Preconco Limited
 Barbados, West Indies

TURKEY

Yapi-Merkezi
 Camlica-Istanbul, Turkey

UAE

Hi-Tech Concrete
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